



**ATKINS**

**Ground Engineering Design and  
Construction Experience in the Region**

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Atkins Middle East

# What are the critical issues?

## **Geotechnical Investigation Practices:**

- Clients often see geotechnical investigations as an exercise that needs to be done without knowing the benefits that can arise
- Quality of investigation practice is very variable
- Geotechnical interpretative reports are often produced by SI contractors
- SI contractors often provide the only supervision themselves
- Required SI standards and methods are often very low

## **Geotechnical Design issues:**

- Contract specifications often demand use of inappropriate codes or mixtures of codes
- Approval bodies often misunderstand the difference between soil and rock (the weak rock : hard soil material range)
- Approval bodies staff generally have not had engineering geological understanding
- Geotechnical design is often overly conservative

# What are the critical issues?

## Things are getting better!:

- The rise of Design & Construct contracts
- Field data of major projects validating geotechnical parameters by back-analysis
- Better SI contractors
- Supervision of SI by the designer is becoming more accepted and even mandated in some cases
- Clients are now better informed and have more experienced staff
- Precedence of works contracts recognising unforeseen ground conditions as a latent condition

# Qatar geotechnical work

Project	Type of Project	SI Scoping Management and Supervision	Desk Studies and Risk Assessments	Geotechnical Interpretation	Geotechnical Design and Advice
Khalifa, Rayan and Al Bustan Road	Infrastructure / Highways	✓	✓	✓	✓
Doha Metro (Tender)	Infrastructure / Heavy Civils		✓	✓	✓
Abu Hamour (Tender)	Infrastructure / Heavy Civils		✓	✓	✓
GEC Doha West	Infrastructure / Highways	✓	✓	✓	✓
Lusail	Infrastructure / Highways		✓	✓	✓
Doha Ceremonial Road	Infrastructure / Highways	✓	✓	✓	✓
Dukhan Highway	Infrastructure / Highways	✓	✓	✓	✓
Education City	Infrastructure/ Structures		✓	✓	✓



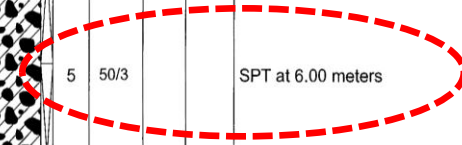
# Investigation Methods Issues



Conventional Wash-Boring

DRILLING EQUIPMENT: Acker AD-II				GROUND WATER			
SIZE & TYPE OF CASING: 5" Steel Casing				DATE	TIME	WATER DEPTH	CASING DEPTH
DRILLING METHOD: Straight Rotary				13-09-2011	10:00	2.60	None
CORE BAR: S.P.T.		LENGTH: 63.50 Kg	BIT: 76 cm	DRILLER: Rahman Malik			
SAMPLER: S.P.T.		WEIGHT: 63.50 Kg	DROP: 76 cm	GEOLOGIST: Abdullah			
DEPTH (m)	DESCRIPTION	PROFILE	SAMPLES		ROCK		REMARKS
			NO.	PENET. BL/15cm	REC. %	RQD. %	
1	Brown, medium dense, clayey medium to fine SAND with sub-angular to sub-rounded gravel of igneous origin.	[Hatched pattern]	1	7 10 13			SPT at 0.00 meters
2	Changing to dense.	[Hatched pattern]	2	40 50/8			SPT at 1.50 meters
3	Brown, very dense, poorly graded GRAVEL of igneous origin with sand & clay.	[Dotted pattern]	3	50/13			SPT at 3.00 meters
4	Brown, very dense, clayey fine to coarse GRAVEL with sand.	[Dotted pattern]	4	50/11			SPT at 4.50 meters
5	Ditto	[Dotted pattern]	5	50/3			SPT at 6.00 meters
6							
7							

Strata boundaries defined by SPT shoe samples



# Investigation Methods Issues



Rotary coring using double tube core barrel

Typical core recovery



# Investigation Methods Issues



Extremely weak, clayey Sandstone  
[comparable samples from wash-boring  
described as dense, clayey Sand]



# Investigation Methods Issues



Extremely weak, sandy Mudrock  
[comparable samples from wash-boring  
described as hard, sandy Clay]

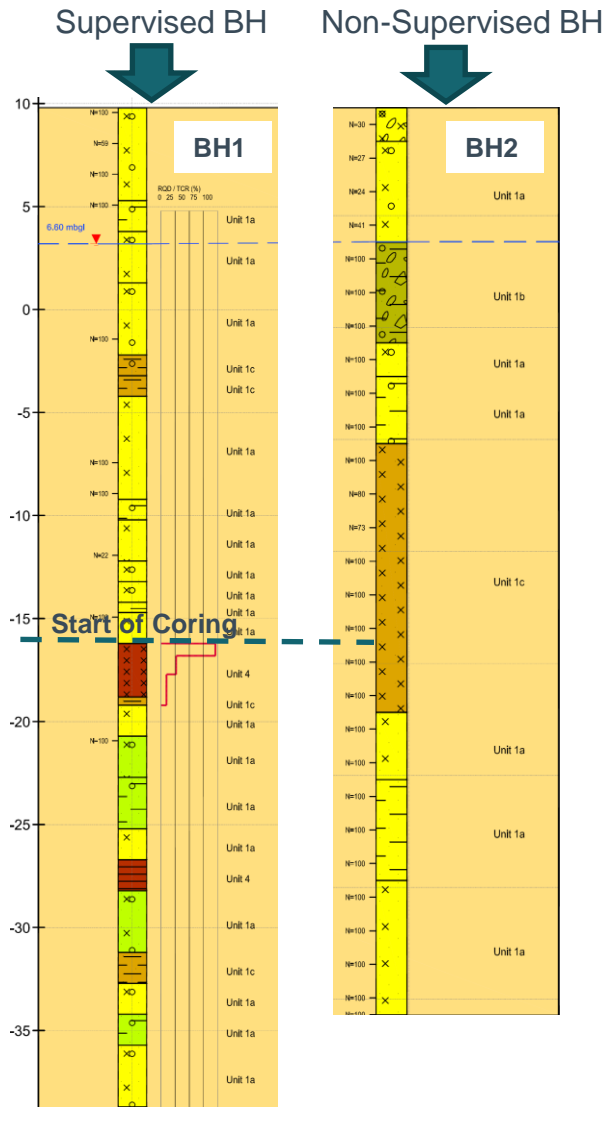


# Investigation Methods Issues

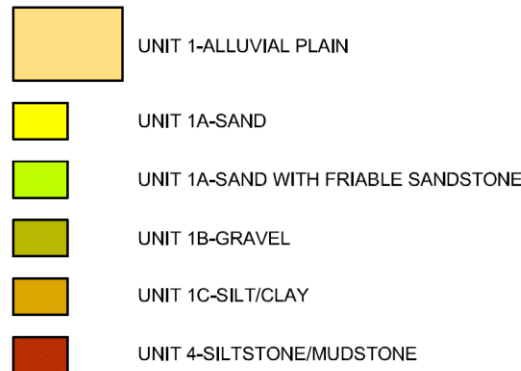


Extremely weak, clayey Sandstone  
[comparable samples from wash-boring  
described as dense, clayey Sand with gravel]

# Investigation Supervision



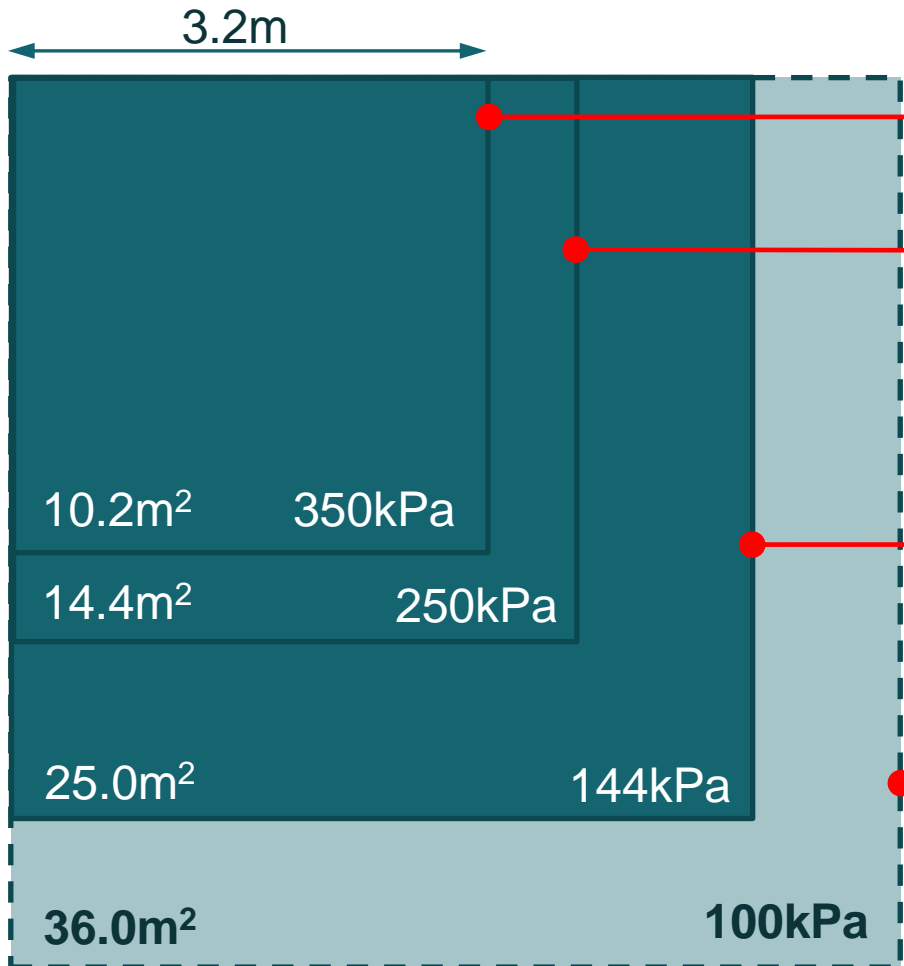
- Two Boreholes (BH) undertaken within 15m, one supervised, one not.
- Wash boring technique used in BH2 – where rock was never established.
- Wash boring not used in BH1 and corable material established after approx 25m depth.
- Difference results in significant difference in piles design.



# Mixing codes

## Impact of mixed codes on design outcome:

Single Type F1 pad: 360 tonnes working load, deflection controlled (<25mm)



## Design progress:

- Use of Burland & Burbridge method (to BS code)
- Requirement to use “stress-strain” method instead, where we used  $E' = 1N_{60}$  for soils with low fines content.  $E'$  corrected to  $E_m$  for the settlement calculation.
- Requirement to use  $E' = 0.7N_{60}$  for all soils with fines content between 10-35%.  $E'$  corrected to  $E_m$  in the calculation.
- $E'$  rather than  $E_m$  should be used, if adopted for this F1 pad this would increase dimension or even need piles.



# Mixing codes

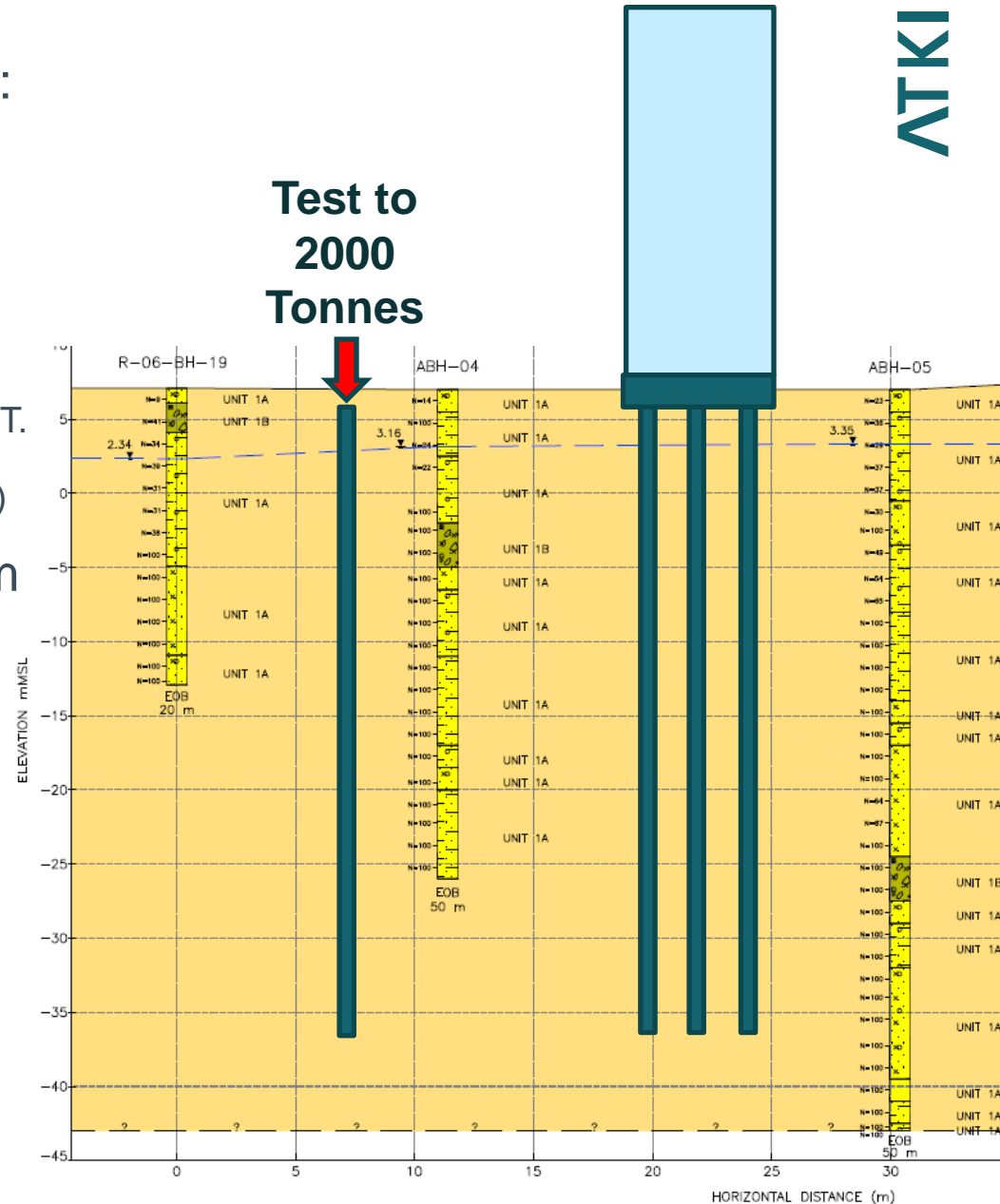




# Assuming ground is soil

Tall building with circular footprint:

- Preliminary pile group design:
  - 43 Piles –  $\varnothing$ 1.2m, L=43m
  - Working load 800 Tonnes
  - Max settlement  $V=48\text{mm}$  ( $H<6\text{mm}$ )
  - Pile Group settlement analysis by PIGLET. Shear modulus derived from  $E'$  (where  $E'=1N$  for sands and  $E'=1.2N$  for gravels)
- Pile load test to  $2.5 \times \text{WL}$  on 43m long pile undertaken
- Actual pile settlement at 2000 Tonnes  $< 13\text{mm}$

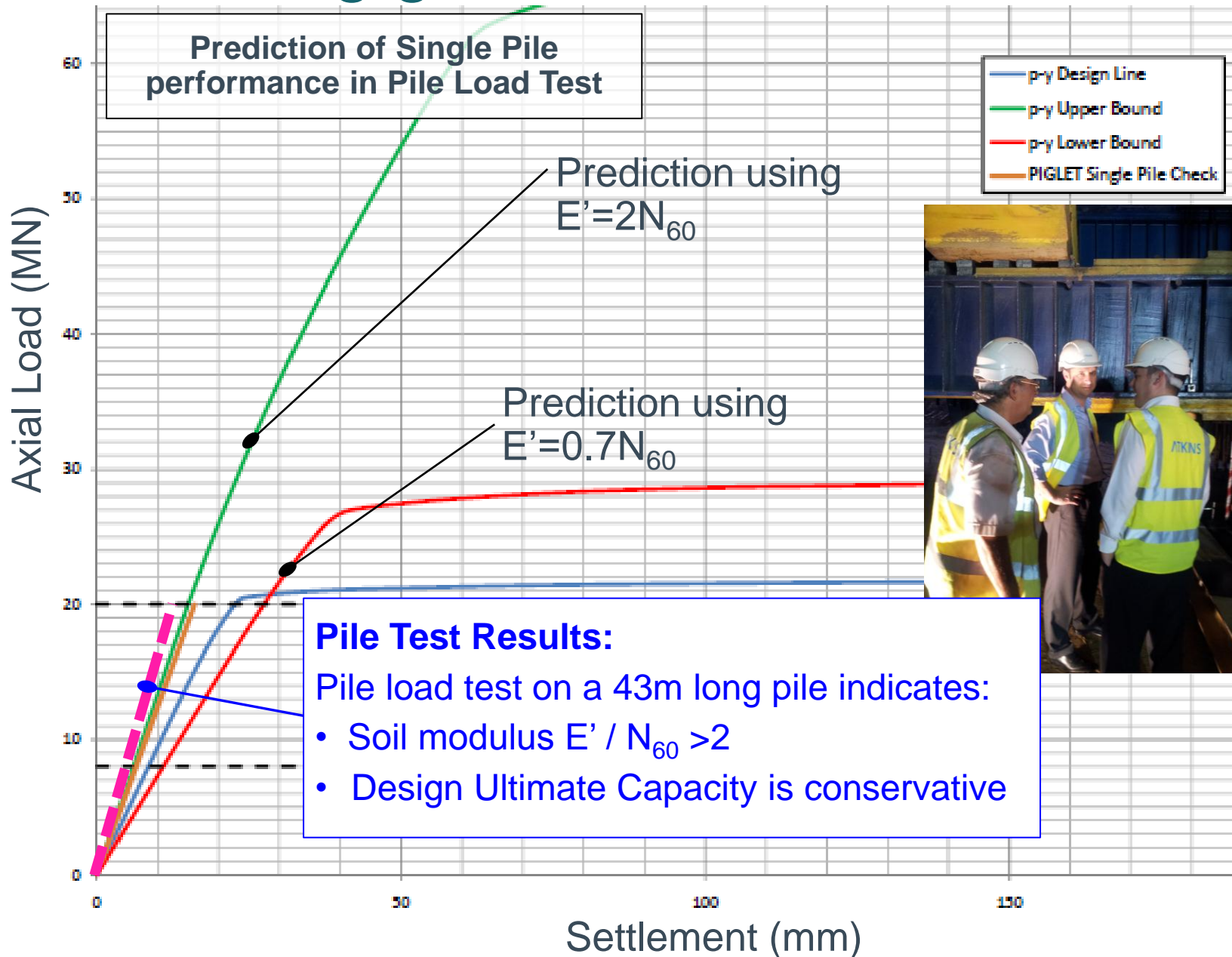


Assuming ground is soil



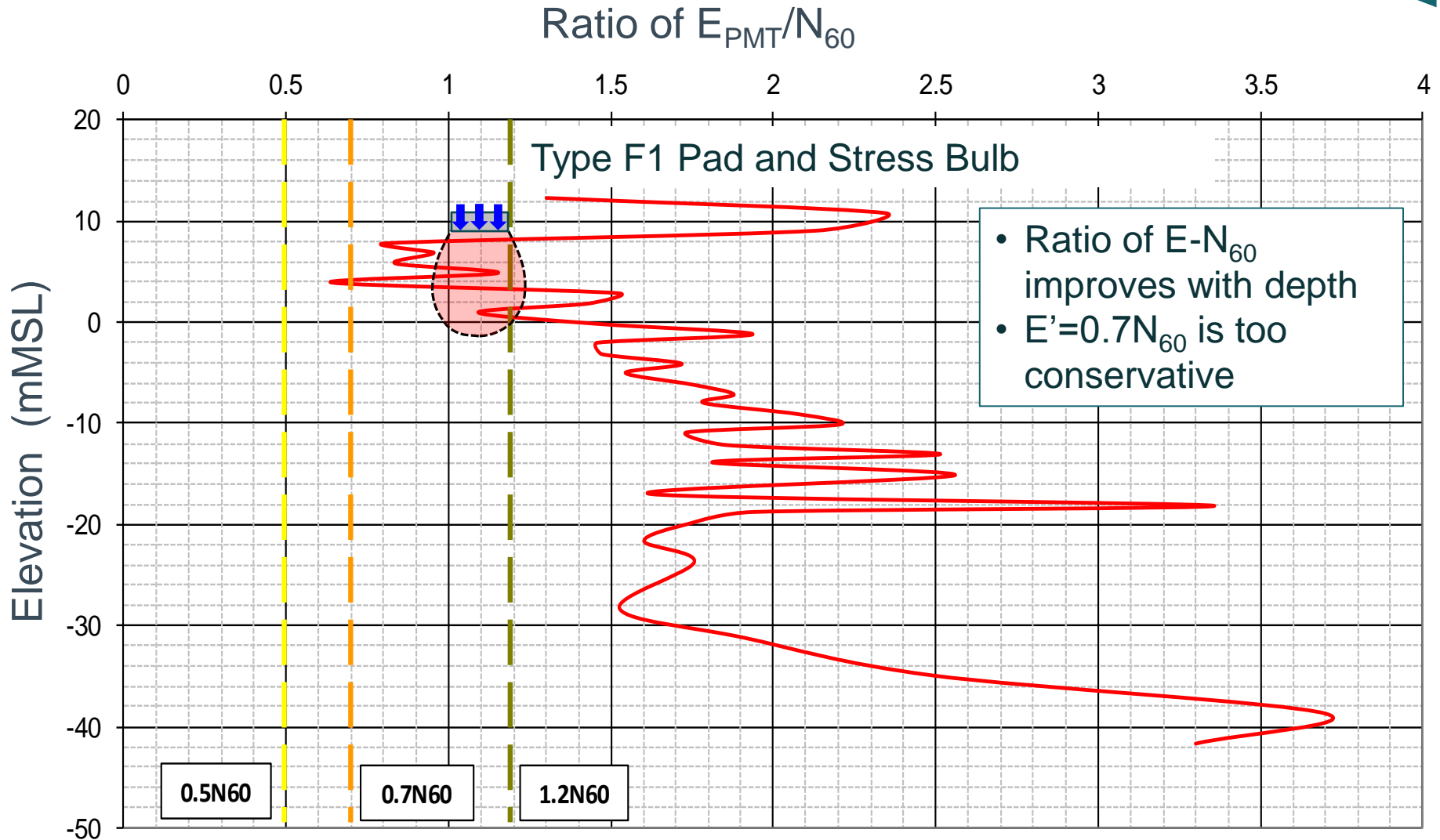


# Assuming ground is soil



# Ignoring field data

Site-wide Pressuremeter test results  $E_{PMT} / SPT N_{60}$  distribution





# Impact on construction





# Use of in-situ field data

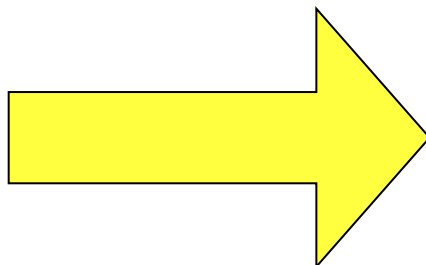
## INVESTIGATIONS:



Boreholes



Laboratory testing



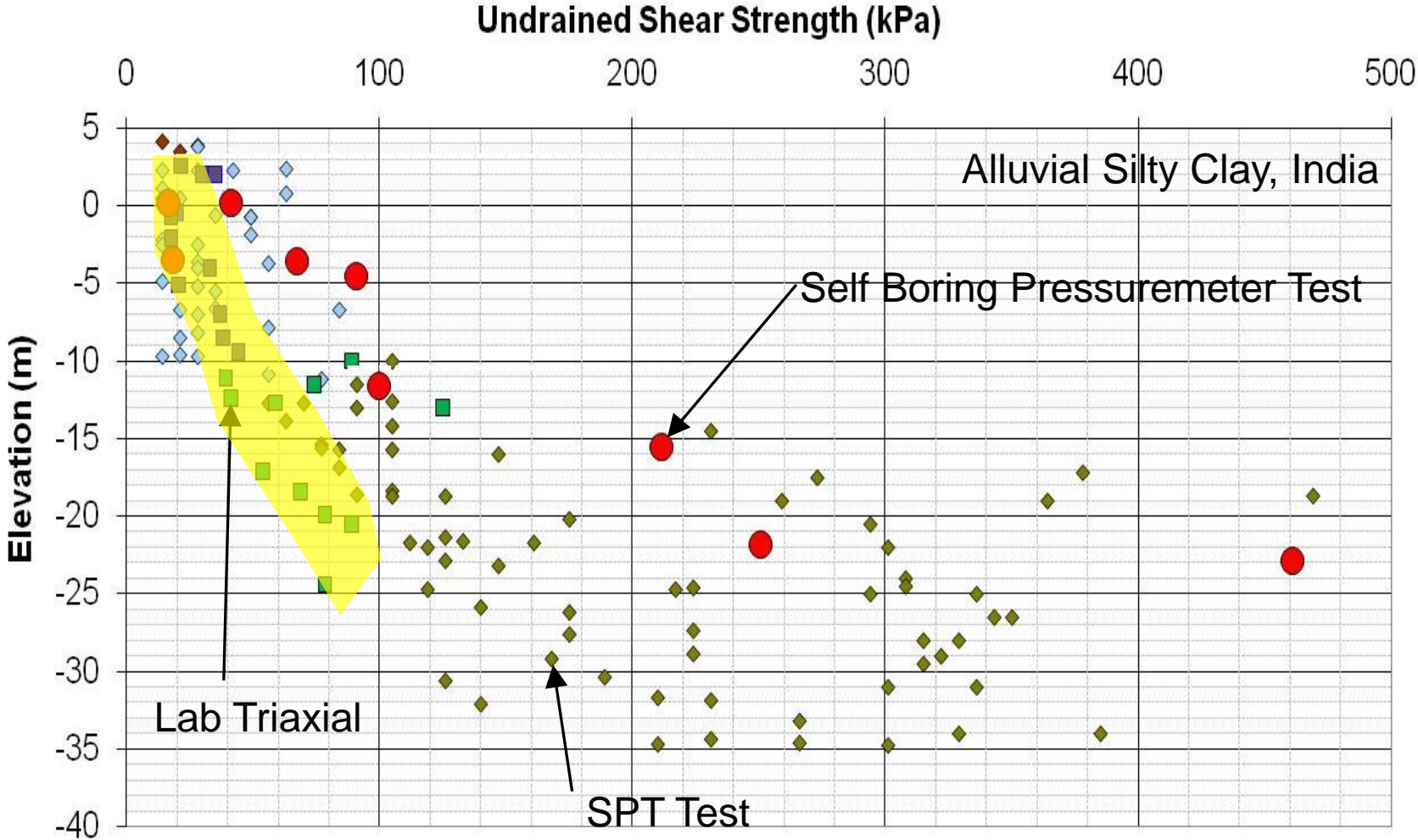
How to interpret?

- Develop geological model
- Design investigations
- Supervise SI
- Correlate in-situ and lab test data and geological model



# Use of in-situ field data

Investment in high quality SI to achieve efficient works design





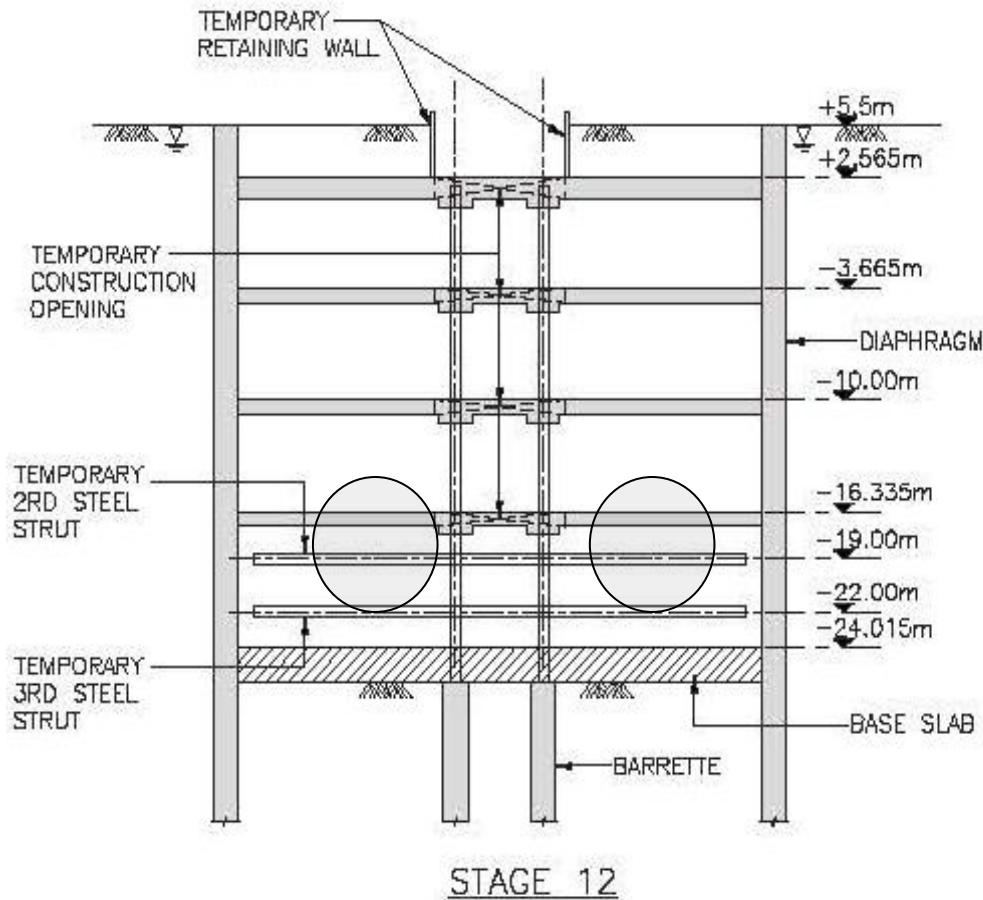
# Tunnel Linings

- Parameter certainty limits reinforcement weight





# Deep excavations



- 12.1 DEWATER TO  $-27.015\text{mMSL}$  AT 1m BELOW EXCAVATION LEVEL.
- 12.2 EXCAVATE TO  $-26.015\text{mMSL}$ .
- 12.3 CONSTRUCT BASE SLAB.
- 12.4 REMOVE TEMPORARY 2ND AND 3RD STEEL STRUTS.
- 12.5 CONSTRUCT PERMANENT COLUMN ROUND STANCHION.
- 12.6 SWITCH OFF DEWATERING SYSTEM AND SEAL TEMPORARY SLAB OPENINGS



Top-Down Metro Station and  
Bottom-up Cross-over Box  
32m deep, 25m wide



# Kolkata – Howrah Maidan Station

- Excavation commencing in main station box

- Crossover box excavation complete & preparing to commence TBM operations

28/06/2012 17:09

- Base slab cast in Crossover





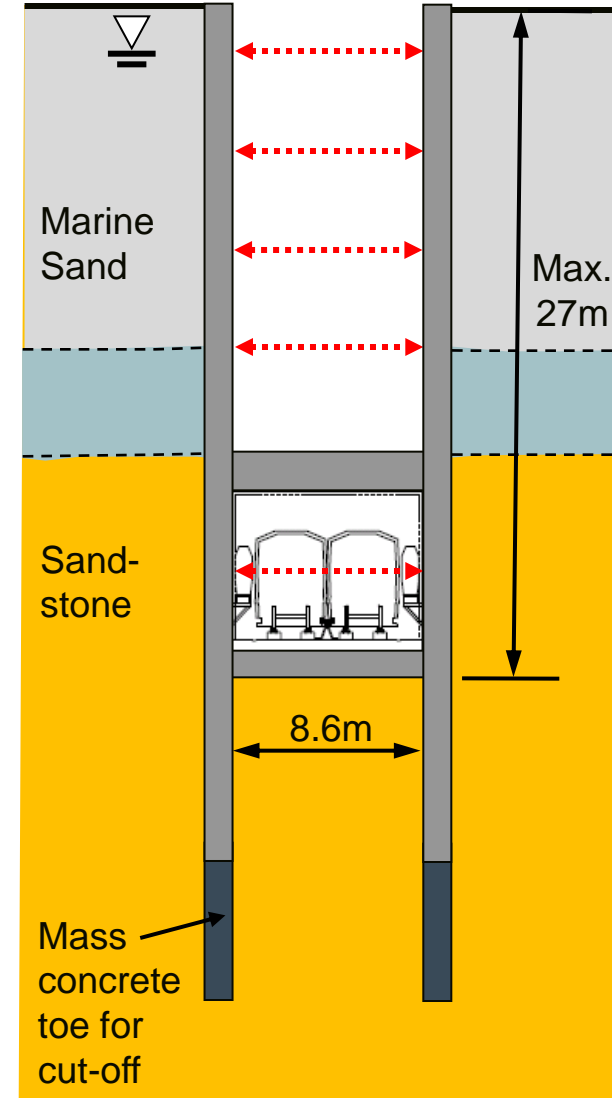
# Back-analysis

## Dubai Metro Cut & Cover Tunnels:

- 4No. Ramps from stations on 4% grade (1.7km)
- Top down construction with permanent Diaphragm Walls
- D-Walls between 0.8m and 1.2m thick
- Temporary struts (Yong Nam type)
- Designed as “Fully fixed” wall-slab joints
- Durability provided by concrete mix design and Contract requirements (<30mm deflection, <0.2mm crack width)



- Observed ground better than suggested by early SI
- This led to campaign of in-situ testing, close monitoring, back-analysis and strut optimisation
- Amended design for RL and changed SI practices for GL
- Atkins supervised GL SI



# Back-analysis

## Dubai Metro Cut & Cover Tunnels:



Multi-level strutting



Slab joint coupler protection

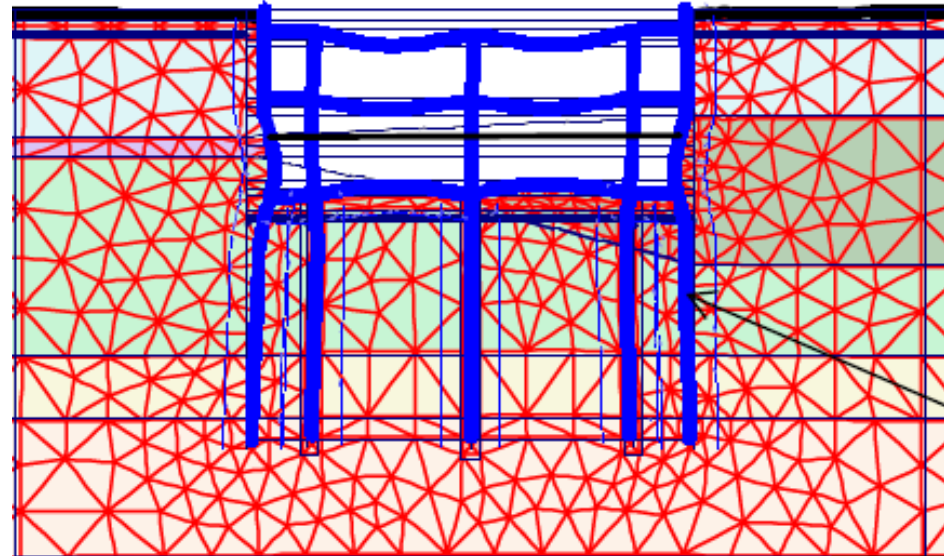
Tunnel portal to trough section with permanent RC struts

Diaphragm wall reinforcement cage being lowered into cut wall slot



# Back-analysis

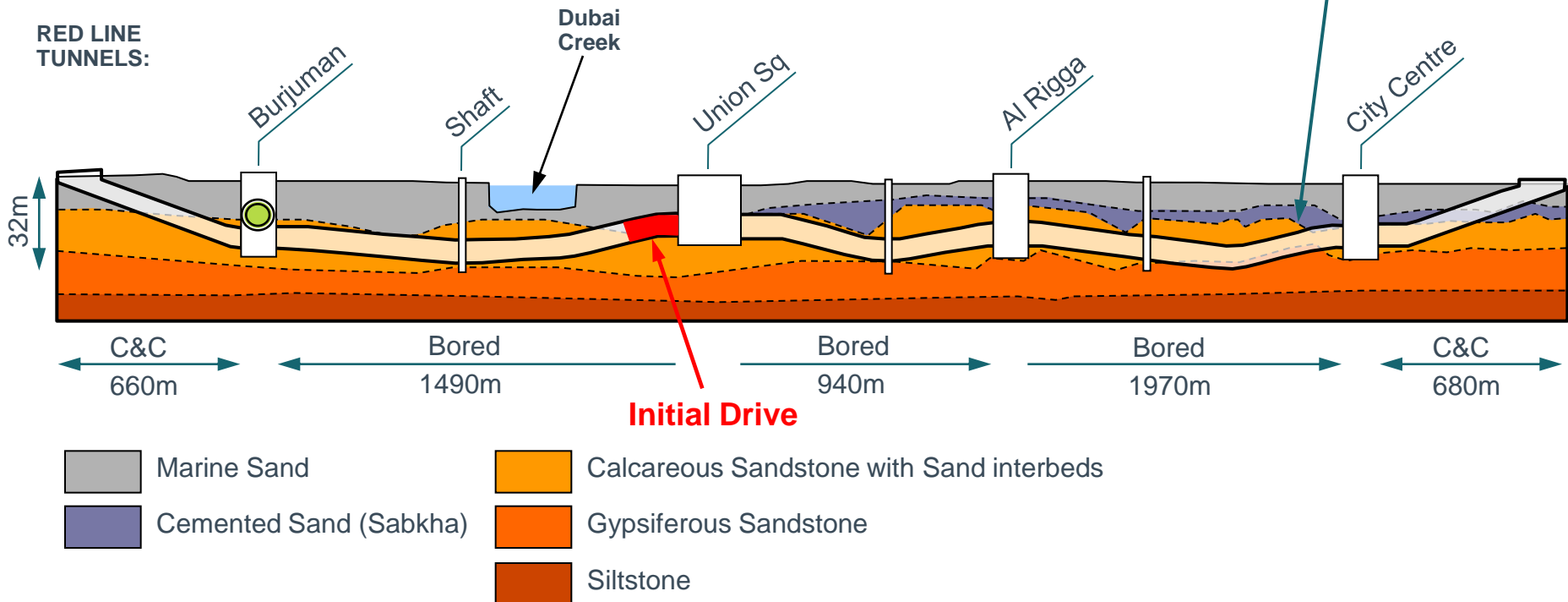
Dubai Metro  
12 Top-Down Metro Stations:  
Union Station



# Back-analysis of tunnelling $V_L\%$

Observational approach – Example: Tunnelling beneath piled buildings

- Initial design of EPB Operating Pressures
- Incorporation of Initial Drive findings
- Validation of predictions

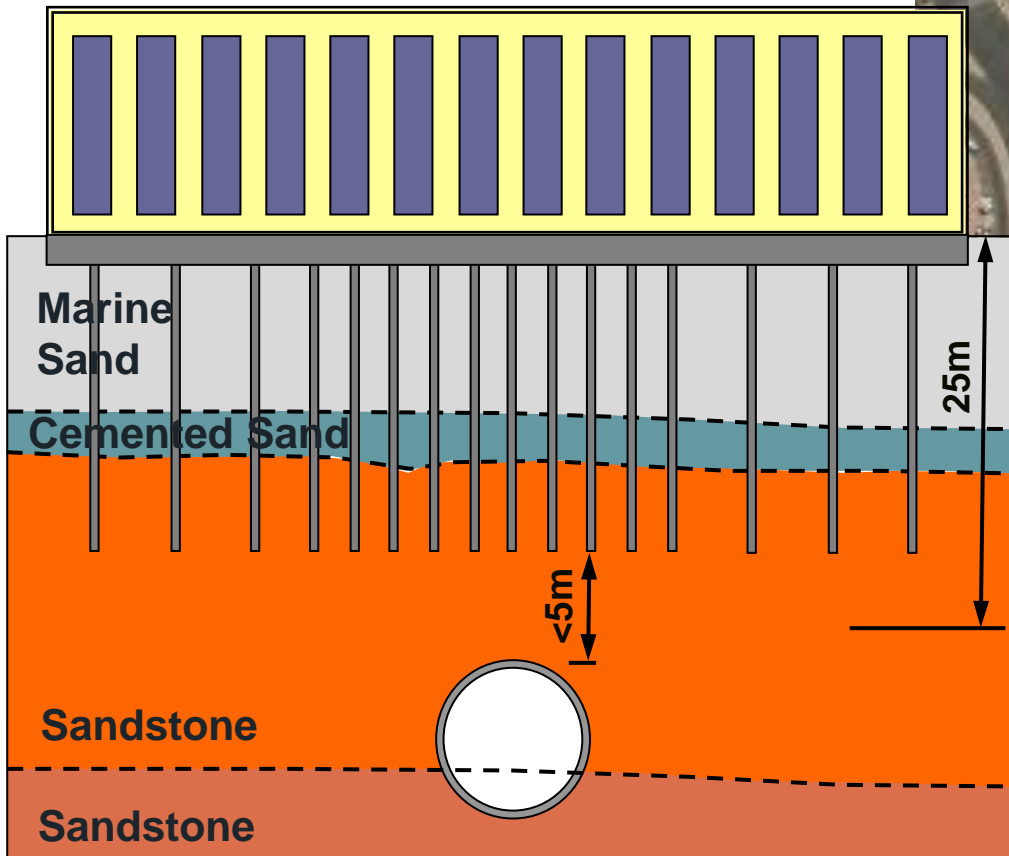




# Back-analysis of tunnelling $V_L\%$

## Dubai Metro – Red Line:

- DNATA Building is at worst risk
- Frame structure over tunnel with cover of 3-5m to pile toes



- Tunnel-Pile interaction analysis to determine tolerable Volume Loss
- $V_L < 0.5\%$  tolerable
- Preferable to manage using TBM Operational Pressures rather than intrusive mitigation

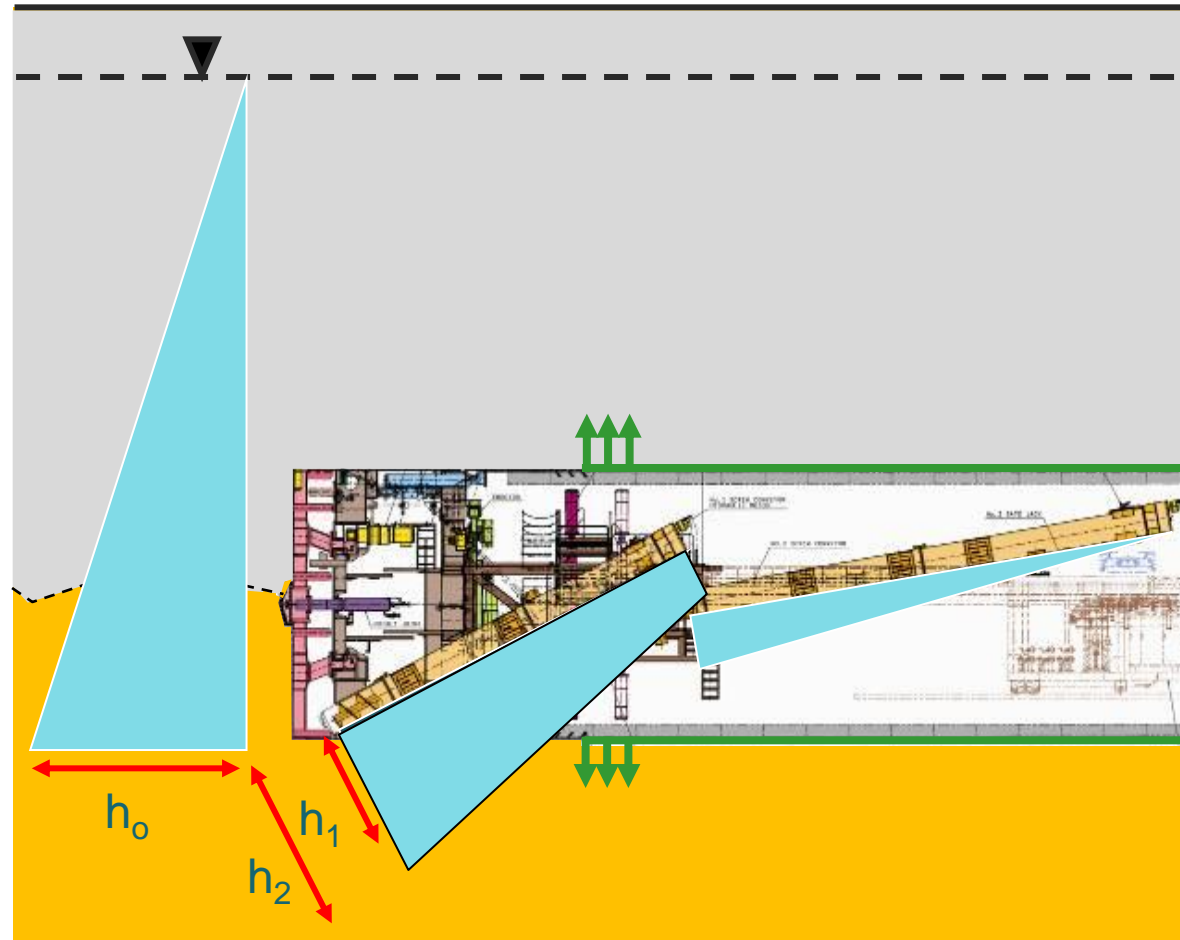


# Back-analysis of tunnelling $V_L\%$

## Detailed Design – TBM face/Annulus grout pressure design

TBM Operational Parameters:

- Intention to limit settlement
- Face pressure based
- Annulus grout pressure
- Pressures can be calculated analytically
- No precedent experience of TBM so Trial Initial Drive important for validation



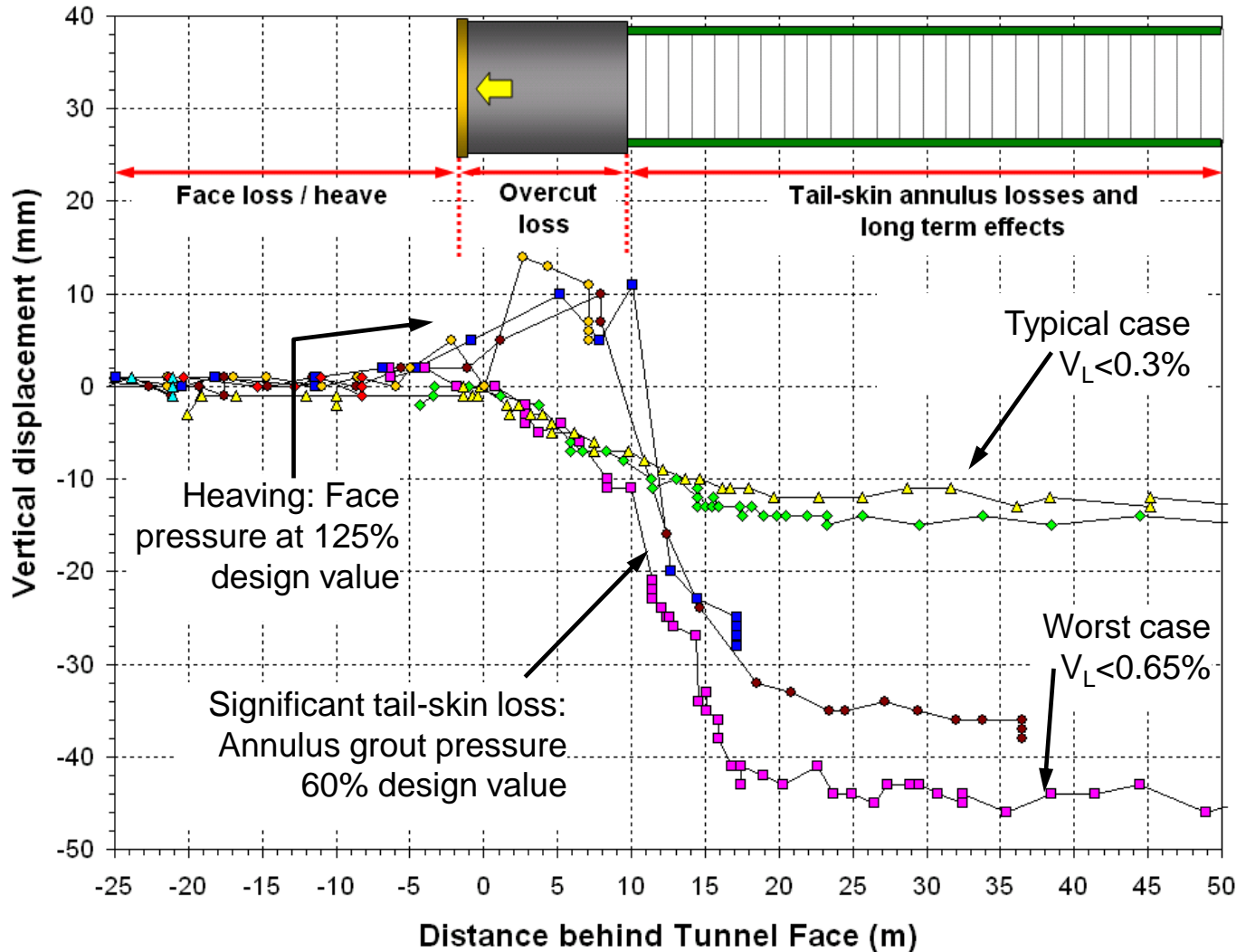
Ratio of  $h/h_0$  is linearly proportional to achievable effective face pressure

# Back-analysis of tunnelling $V_L\%$

RED LINE

100m Initial Drive:

Settlement data for mixed face tunnelling



# Back-analysis of tunnelling $V_L\%$

FEM Analyses (FLAC3D and PLAXIS3D)

Back-analysis of Initial Drive  
& sensitivity analysis

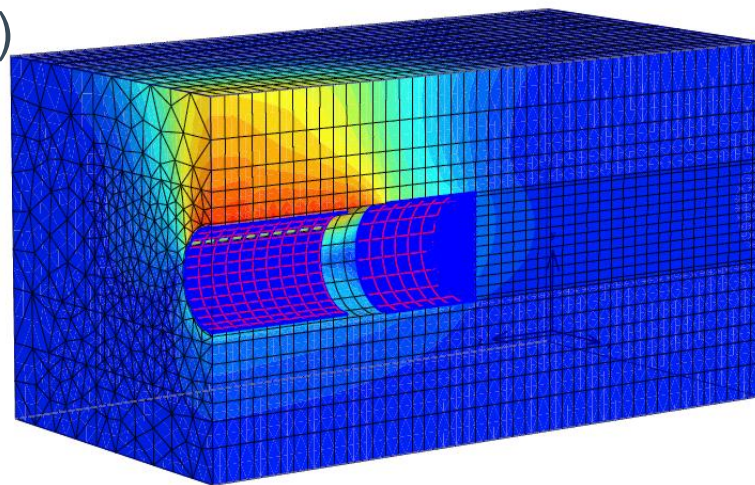
Calibrated models for:

- RL validation of calculations
- GL design to calibrate the analytical calculations
- Reassessment of DNATA

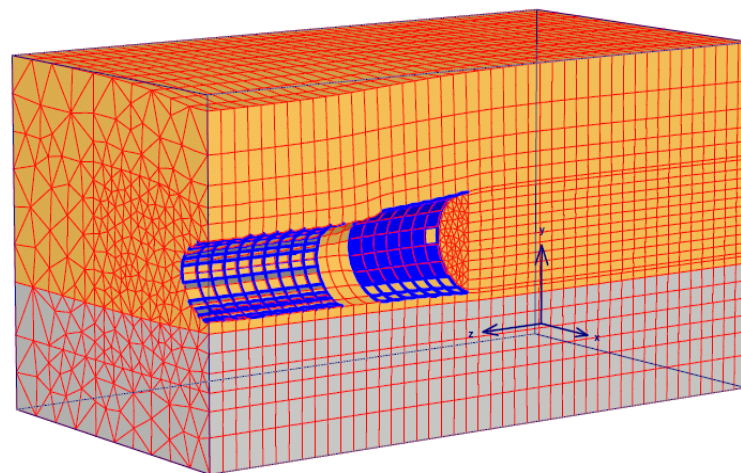
Analytical calculations (FoS 1.2)  
are reasonably conservative

Gave confidence for GL design  
in extensive mixed conditions

DNATA: We reduced pressures:  
Settlement was negligible



Displacement contours

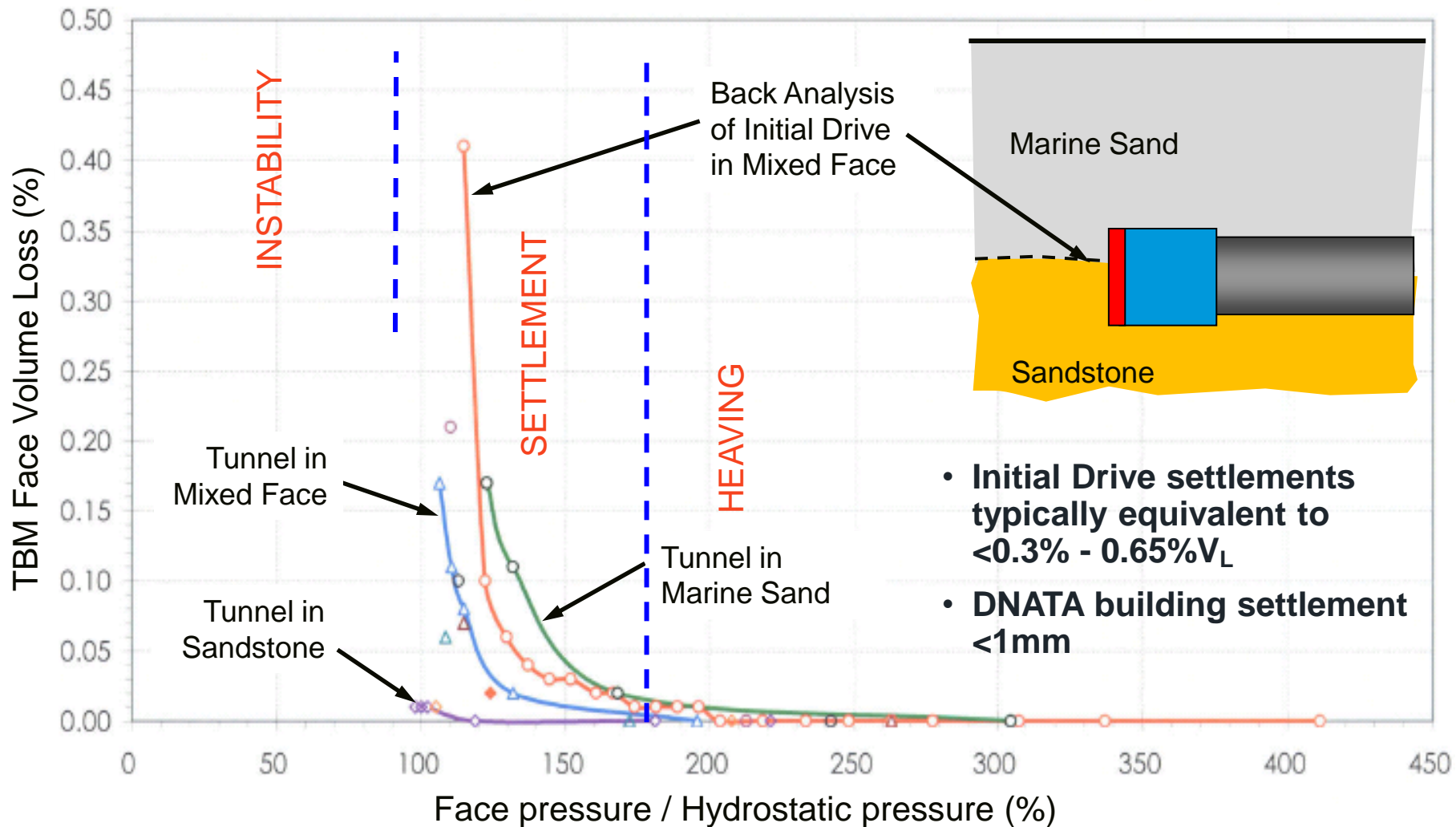


Deformed mesh



# Back-analysis of tunnelling $V_L\%$

FEM Analyses (FLAC3D and PLAXIS 3D):





# Back-analysis of tunnelling $V_L\%$





# Conclusions

## Future trends:

- Better understanding of the geotechnical characteristics of the weak rocks in the region
- Improving geotechnical investigations practices
- Cleaner application of codes (EN introduction is significant)
- More cost-effective projects